

APPLICATION  
FOR  
UNITED STATES LETTER PATENT

Applicant(s) Name: SYRACUSE UNIVERSITY

**Inventor:** Laurel H. Carney

Address: 503 Standish Drive  
Syracuse NY 13224

**Inventor:** Michael C. Anzalone

Address: 115 Remington Avenue, Apt. D.  
Syracuse NY 13210

Title: System and Method for Detecting A Narrowband Signal

Docket No. 156 P 023

I hereby certify that this paper (along with any paper referred to as being attached or enclosed) is being deposited with the United States Postal Services on the date shown below with sufficient postage as Express Mail No. EV191632268US in an envelope addressed to Mail Stop Patent Application Commissioner for Patents PO Box 1450, Alexandria, VA 22313-1450 on July 31, 2003

  
Ann R. Miller

Date: July 31, 2003

Patent Application Of: Laurel H. Carney and Michael C. Anzalone

For: System and Method for Detecting a Narrowband Signal

#### CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] The present application claims priority to U.S. Provisional Application Serial No. 60/400,359 filed July 31, 2002, entitled "An Algorithm for Detection of a Narrowband Signal of Known Frequency in a Wideband Fluctuating Noise," hereby incorporated by reference.

#### STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

[0002] The U.S. Government has a paid-up license in this invention and the right in limited circumstances to require the patent owner to license others on reasonable terms as provided for by the terms of Grant No. R01 01640 awarded by National Institutes of Health—National Institute on Deafness and Other Communication Disorders.

#### BACKGROUND OF THE INVENTION

##### 1. Field of Invention

[0003] The present invention relates to the detection of narrowband signals and, more specifically, to a system and method for detecting of a narrowband signal of known frequency in a wideband fluctuating noise.

##### 2. Description of Prior Art

[0004] The detection of a narrowband signal amidst wideband noise is an important feature in communication devices ranging from cellular telephones to human hearing aids. To detect a target signal, systems typically use a filter tuned near the frequency of the target signal that rejects the remaining noise frequencies. The ability of such a system to detect a target signal is often affected by the signal-to-noise ratio (SNR), and the effectiveness of such

a system is susceptible to fluctuations in the noise level that causes fluctuations in the output energy of the filter.

[0005] Other systems for detecting a narrowband signal use previously determined information about the noise to construct a filter that is matched to the properties of the noise, such as a Wiener filter. A system such as this depends on prior knowledge of the properties of the noise, however, and is ineffective when the noise varies or is indeterminate. Some systems, such as a Kalman filter, depend on a running estimate of the properties of the noise and use a time-varying filter to optimize the signal-to-noise (SNR) ratio. These systems, however, require sophisticated modeling of the noise and require complex algorithms.

[0006] Another large class of signal detectors correlate the incoming signal and noise with a template for the target signal. These detector systems require knowledge of the incoming signal characteristics and cannot always discern signals that do not have perfect tones or long-term temporal stationarity.

### 3. Objects and Advantages

[0007] It is a principal object and advantage of the present invention to provide a system and method for detecting a narrowband signal in wideband noise having fluctuating characteristics, such as amplitude.

[0008] It is an additional object and advantage of the present invention to provide a system and method for detecting a narrowband signal that does not require prior knowledge of the properties of the noise.

[0009] It is a further object and advantage of the present invention to provide a system and method for detecting a narrowband signal that is not a perfect tone or does not have long-term temporal stationarity.

[0010] It is another object and advantage of the present invention to provide a system and method for detecting a narrowband signal that does not require lengthy processes or sophisticated algorithms.

[0011] Other objects and advantages of the present invention will in part be obvious, and in part appear hereinafter.

#### SUMMARY OF THE INVENTION

[0012] The present invention comprises the detection of a known frequency, *i.e.*, a target signal, in wideband noise using temporal information extracted from the signal using a cross-frequency, cross-correlation. A target signal is detected in wideband noise by a running cross-correlation of the output of two narrowband filters, one having a center frequency below the known frequency of the target signal, and the other filter having a center frequency above the frequency of the target signal. The frequencies of the two filters are selected so that the phases of their transfer functions differ by 180 degrees relative to each other about the frequency of the target signal. The outputs of the two filters are processed by a saturating nonlinearity function, such as the signum function, to “clip” the amplitude fluctuations of the filter responses without affecting the times of the zero-crossings. The saturated outputs of the two filters are then compared using a running cross-correlator (or a point-by-point multiplication of the two signals, followed by a low-pass filter). If the target signal is present, the output of the running cross-correlator will decrease due to the 180-degree phase difference between the responses of the two filters at the signal frequency, an effect termed “phase opponency.” With appropriate thresholding, the reduction in the output of the running cross-correlator signals indicates when the target frequency is present.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0013] Fig. 1 is a schematic of a detector according to the present invention.

[0014] Fig. 2 contains graphs of the magnitudes and phases of the transfer functions of two filters selected according to the present invention to detect a 900 Hz target signal.

[0015] Fig. 3 contains graphs comparing the half-wave rectified responses of two filters chosen according to the present invention in the presence of (a) noise and (b) noise plus a 900 Hz target signal.

[0016] Fig. 4 is a series of graphs comparing, over time, (A) a 900 Hz target signal, (B) Gaussian noise, (C) the output of a running cross-correlator according to the present invention, and (D) the output of the detector of the present invention.

[0017] Fig. 5 is a series of graphs comparing, over time, (A) a 900 Hz target signal, (B) wideband noise having fluctuating amplitude, (C) the output of a running cross-correlator according to the present invention, and (D) the output of the detector of the present invention.

#### DETAILED DESCRIPTION

[0018] Referring now to the Figures, wherein like parts are referred to by like numerals throughout, there is seen in Fig. 1, a detector 10 according to the present invention for indicating the presence of a target signal having a predetermined frequency in wideband noise of fluctuating amplitude.

[0019] Detector 10 comprises two narrowband filters 12 and 14 having center frequencies F1 and F2. Frequencies F1 and F2 are selected to be above and below the target signal frequency and differ by 180 degrees about the frequency of the target signal and can be derived analytically for a given filter transfer function. Filters 12 and 14 can comprise two band pass filters, or a low-pass and a high-pass filter, as long as the orders of the filters are sufficient to create a 180-degree phase difference at the target signal frequency. The magnitudes and phases of the transfer functions of filters 12 and 14 used to detect a 900-Hz signal, for example, are illustrated in Fig. 2.

**[0020]** The outputs from filters 12 and 14 are processed by saturating non-linearity components 16 and 18 to remove amplitude information. The saturating nonlinearity components 16 and 18 creates a signal output that goes no higher than +1 and no lower than -1. For any positive value on the input, the output is set to +1 and for any negative input, the output is -1. Thus, after the saturating nonlinearity, the signal is dominated by +1, -1 and the zero crossings, and is no longer affected by changes in the signal energy. After saturation, the timing of the zero crossings is determined by the positive and negative fluctuations in the input signal and the frequency and phase information in the input signal is all that passes. The saturating non-linearity components 16 and 18 can be accomplished by a simple circuit, such as a very high-gain amplifier followed by a pair of limiters (e.g. a diode circuit), or by software programmed with a signum function, for example.

**[0021]** The saturated non-linear outputs are then compared by a cross-correlator 20 that measures the correlation of the signals as a function of time. Cross-correlator 20 can comprise a programmed software function, a multiplier, or modulator circuit designed from transistor circuitry.

**[0022]** The output from correlator 20 is then passed through a low-pass filter 22, forming what is referred to as a running cross-correlator 24. Low-pass filter 22 has a cut-off frequency that determines the integration time of running cross-correlator 24, and the output of low-pass filter 22 at any one point in time depends on recent history (depending on the corner frequency of low-pass filter 22), as opposed to depending only on the input at that moment. Detection 28 of the target signal occurs when the output of low-pass filter 22 drops below a predetermined threshold value 26 (see Fig. 4C). Lower cutoff frequencies of low-pass filter 22 results in a more sensitive detector, but in a slower response time. Thus, the

desired response time and sensitivity must be considered when determining the cut-off frequency of low-pass filter 22.

[0023] The half-wave rectified responses of filter 12 and 14 to (a) noise and to (b) noise plus a target signal (*e.g.*, a frequency of 900 Hz) are shown in Fig. 3. The response of filter 12, for example, is shaded light gray in both panels, and the response of filter 14, for example, is shaded dark gray. In the presence of wideband noise, see Fig. 3a, the responses of filters 12 and 14 are partially correlated, due to the overlap of the transfer functions of filter 12 and 14. The times that both filters 12 and 14 respond simultaneously are shaded black in Fig. 3 for the purposes of illustration. In the presence of wideband noise, the partially correlated signals from filters 12 and 14 result in a positive response of running cross-correlator 24. In response to the wideband noise plus the target signal frequency, the responses of filters 12 and 14 are drawn out-of-phase, see Fig. 3b), resulting in a reduced response from running cross-correlator 24.

[0024] As an example, the response of detector 10 to a signal of 900 Hz in Gaussian noise can be seen in Fig. 4, which contains corresponding graphs A-D illustrating the various inputs and outputs of the present invention plotted correspondingly over time. More particularly, graph A of Fig. 4 shows the presence of several narrowband 900 Hz tones comprising the target signal. Graph B depicts 3 kHz bandwidth Gaussian noise, where the SNR is equal to 28 dB. Graph C shows the output of running cross-correlator 24 to the combination of background noise and the 900 Hz tones. When the output of running cross-correlator 24 dips below a threshold (the dotted line in Fig. 4C), the response signal is set to one, as seen in 4D. Fig. 5 depicts the various outputs of present invention when a 900 Hz signal is contained within wideband noise having fluctuating amplitude.

[0025]                    Detector 10 according to the present invention thus signals the presence of a known narrowband frequency within a wideband signal through the identification of a reduced response of running cross-correlator 24, as compared to the response of running cross-correlator 24 to a wideband signal containing only noise. As the reduced response of running cross-correlator 24 occurs independently of the amplitude information in the wideband noise, fluctuations in the amplitude of the noise will not adversely impact the effectiveness of detector 10.